Example Problem 1. F	igure 2. Single sh	ear. Side S4S 2x1 o.c. in row. 2 rov	0, Main S4S 3	x10		
Notes		n: main member =		r = 0		
	Except for the yell cells, this spreads to prevent accider formulas.	heet is protected	Engineering Proper Species D Doug Fir-Larch Eastern Hemlock Eastern Spruce Hem-Fir	ensity Mod (G) No. 1 .50 1,700,000 .41 1,100,000 .41 1,100,000	No. 2 N 1,600,000 67 1,100,000 350	Tensile (F <sub>i</sub> ) lo. 1 No. 2 5 575 0 275 0 275
Inside the second secon			Red Oak South'n Pine Westn Cedar Westn Hemlock White Oak	.55 1,700,000	1,600,000 1,000,000 4 1,000,000 30	300
load: lateral (L), withdrawal (W), load in side grain (s) or end grain specific gravity (g) or dowel bear side member wood (w) or steel ( standard lag screw (s) or threade lag screw shank diameter (inche	i (e) s ing (b) g s) w		Length I	ard Lag Screw S ",1 1/2" 2",2 '4" - 1/2" 1/4" -		4" - 12" 1/4"-1 1/4"
ing screw length (inches) if W or C in E24, threaded penetri if C in E24, total penetration dowel bending yield (psi)	L = 4.00		Fill in turquois they are to be	e column witi used instead	n dowel bea d of specific	ring strengt
side member thickness (inches) main member thickness (inches) side member specific gravity main member specific gravity	$L_s = 1.50$ $L_m = 2.50$ $G_s = 0.5$	side m	ember dowel t ember dowel t ember dowel t nember dowel	bearing =	F <sub>es</sub> F <sub>es</sub> F <sub>es</sub>	5600 3650 5600 ### 5600
load to grain side member <sup>o</sup> load to grain main member <sup>o</sup> load to wood surface <sup>o</sup>	G <sub>m</sub> = 0.5 s = 0 m = 0 á = 0 â = 90	) main n ) main n	nember dowel	bearing = bearing =	F <sub>em</sub> F <sub>em</sub> F <sub>em</sub>	3650 3650 5600 ###
of lag axis and wood surface <sup>c</sup> washer thickness if used length of tip effective total penetratio	w = 0.125	use	d F <sub>es</sub> = d F <sub>em</sub> = 1.00 (la	5600 5600 teral)		
effective threaded lengt effective screw length root diameter diameter for lateral form	2.281 2.156 0.265	C <sub>eg</sub> =		thdrawal)		
		R <sub>e</sub> =	1	R <sub>t</sub> = 1.6	67	
	k = 1.122 K = 1	Load Du permane occupan snow construc	cy live	Ref.3) 0.9 1 1.15 1.25		
$      Yield Mode \ I_s  Z = \\       Yield Mode \ I I \ I_s  Z = \\       Yield Mode \ IV  Z = $	560 pound 260 pound 200 pound	s	ake	1.6		
BASIC LATERAL DESIGN VALU	200 pound					
Number of Lags in Joint	= 6	DATA IN BOX B	ELOW APPLIE			ONLY
Load Duration Factor, Wet Conditions Factor,	C <sub>D</sub> = 1.15	number number lag spac	of rows = ags in a row = ing in row (inches) mber mod. of elast	=	2 3 3.0 1.7	
	C <sub>g</sub> = 1.00 C <sub>gf</sub> = 1.00	main me	mber mod. of elast mber gross area (s nber gross area (s 41335 1.00421	sq. in.) = q. in.) =	1.7 23.12 13.87 Factors, C <sub>1</sub> (F	Ref.4)
Lateral Design Value One Lag Lateral Design Value All Lags	170 pound 1020 pound	m = R <sub>EA</sub> = s	0.91238		(inches) ,4	factor 1.5 1.4 1.3 1.2
NET SECTION CALCU	LATIONS FOR A	LOWABLE TENS		10 12 All 5		1.1 1.0 1.0
Tensile Stress Main Mei Tensile Stress Side Mer Size Factor Main Memb Size Factor Side Membe Temperature Factor,	mber, F <sub>t</sub> = 675 er, C <sub>f</sub> = 1.1		Tension Load actual width of ma actual width of sic net area main me net area side men	ain member = le member = mber =	9.25 9.25 21.34 12.75	nches sq. in.
Design Value for Main M Design Value for Side M	15850 1ember = 9470	pounds tension pounds tension				

This spreadsheet is provided for illustrative teaching purposes only, and is not intended for use in any specific project. Anyone making use of the information contained in this spreadsheet does so at his/her own risk and assumes any and all resulting liability arising therefrom.